

THERMAL EFFICIENCY ENHANCEMENT OF GASOLINE ENGINE

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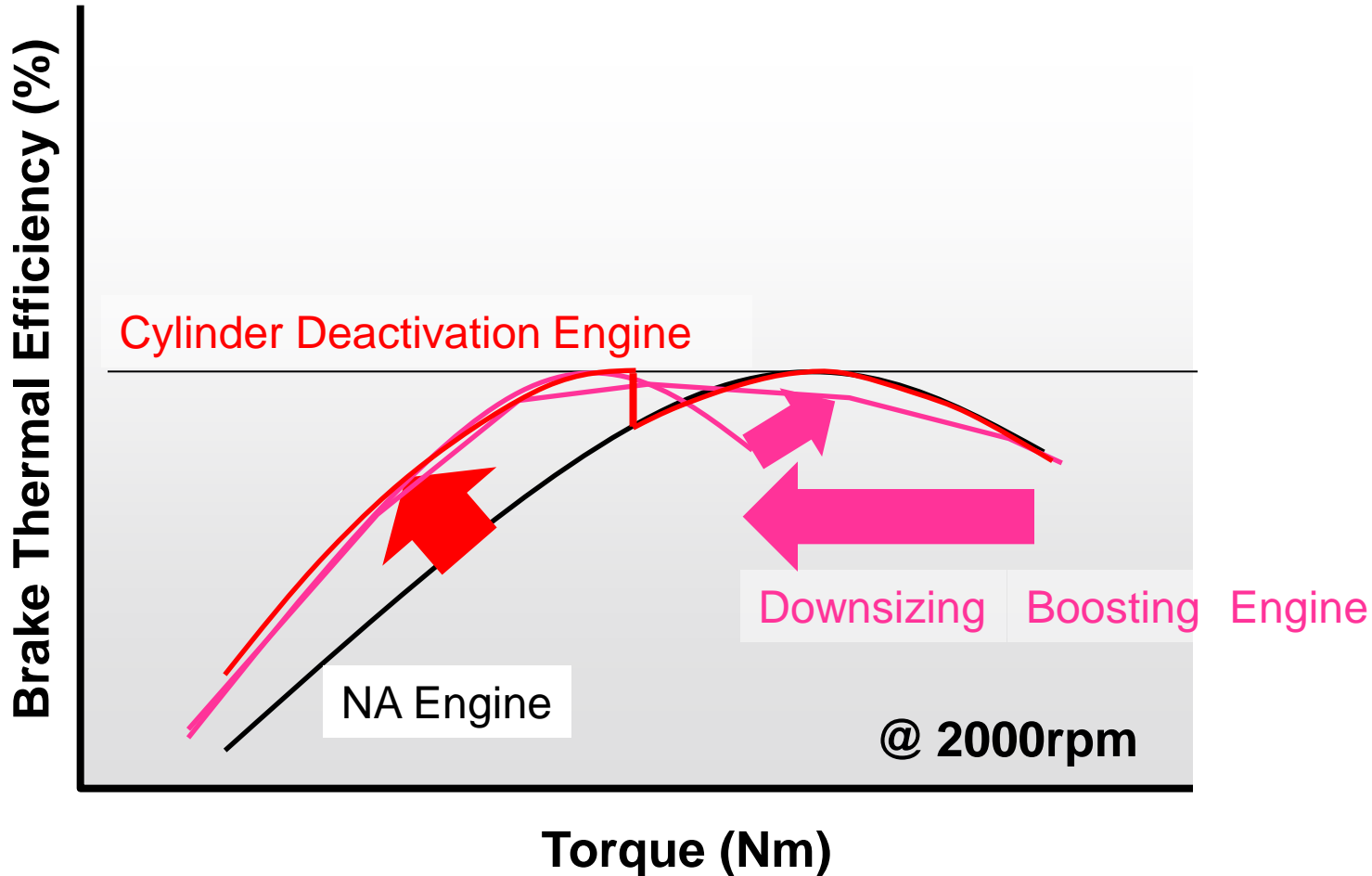


3. How to Achieve Brake Thermal Efficiency 45%

<SAE_PAPER 2015-01-1263>

4. Conclusion

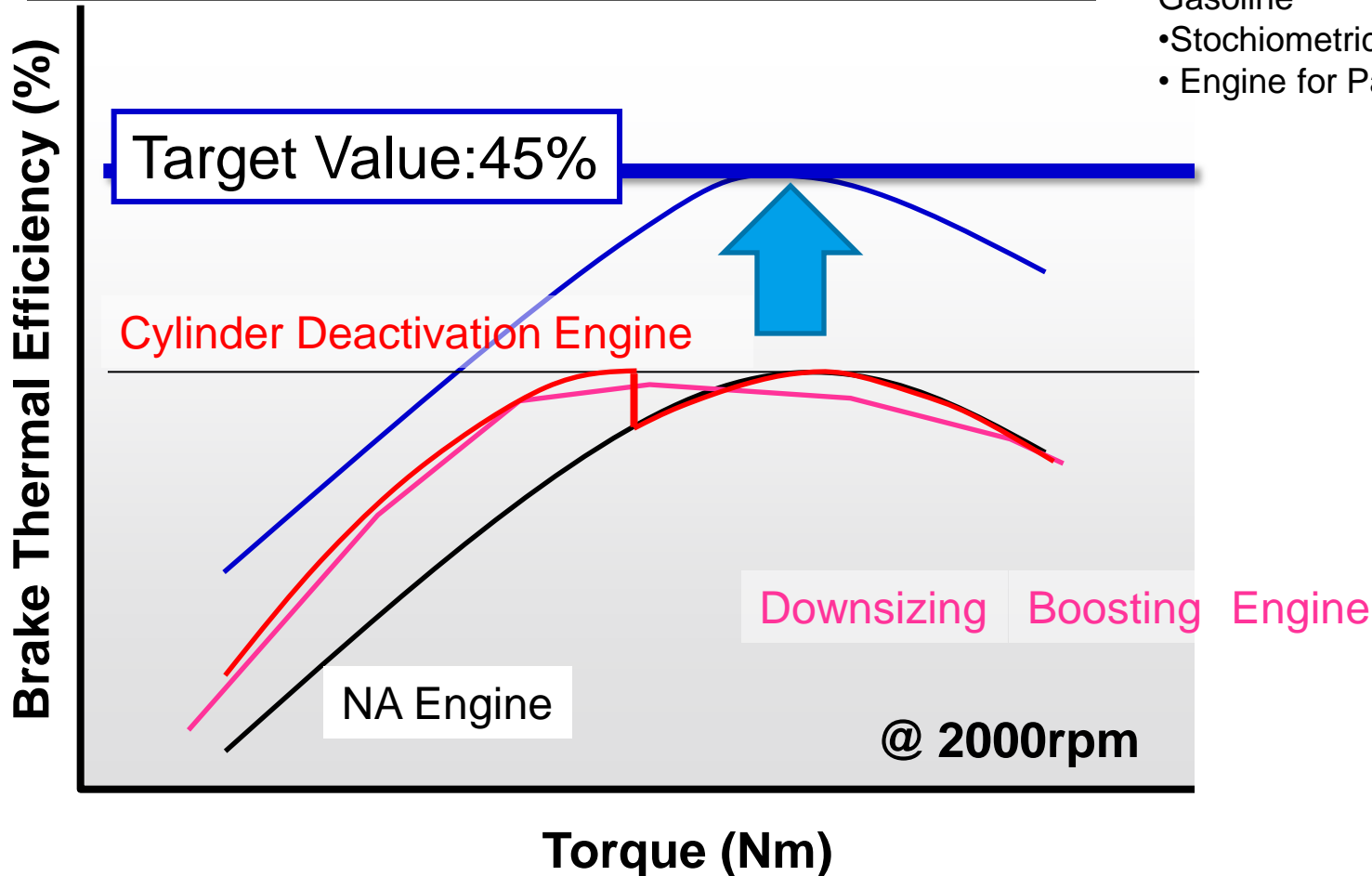
Intended Direction of This Research



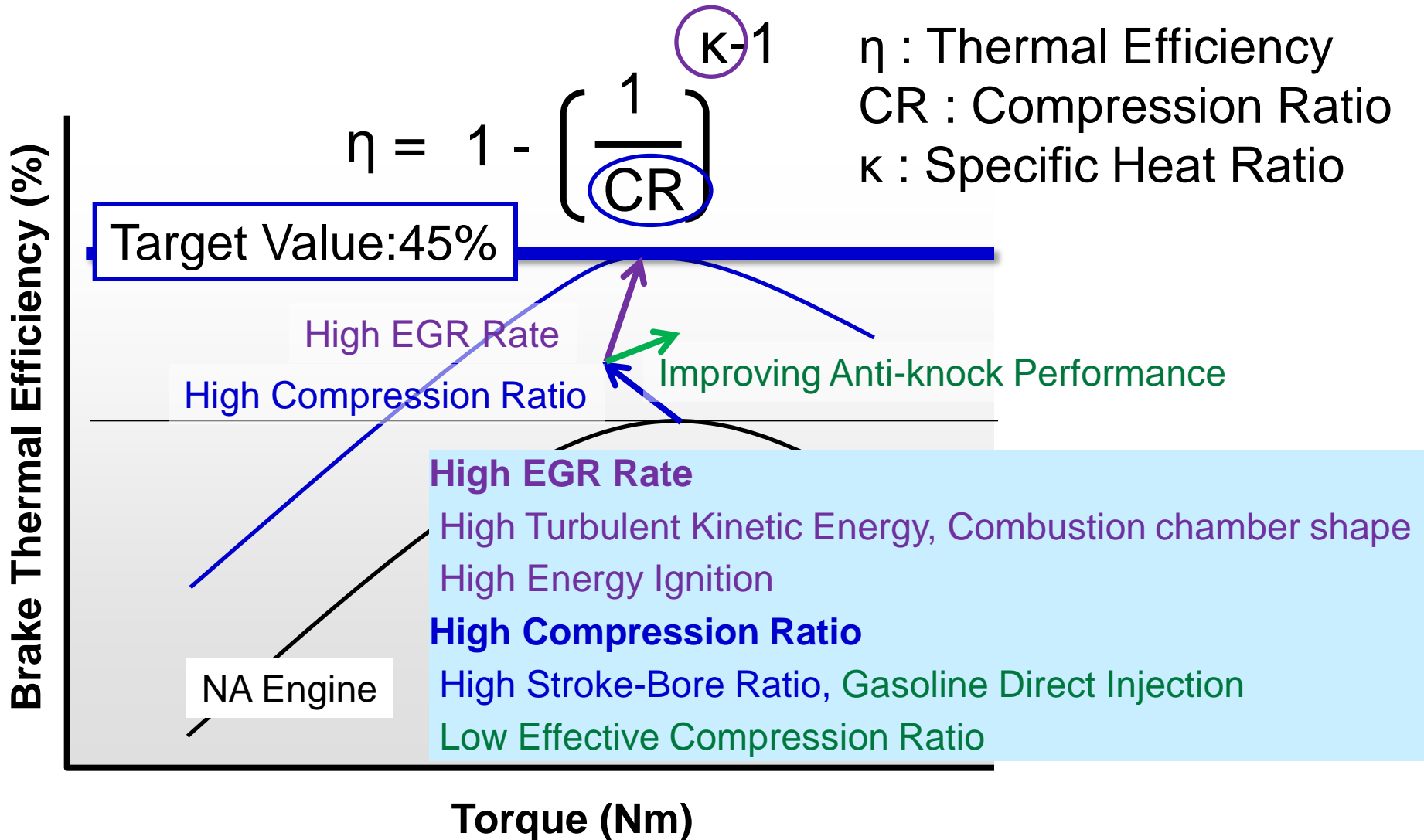
Intended Direction of This Research

Aim of This Research:
Improvement of Maximum Brake Thermal Efficiency

- Under Following Condition
- 91 Research Octane Number Gasoline
 - Stoichiometric Air/Fuel(A/F) Ratio
 - Engine for Passenger Car



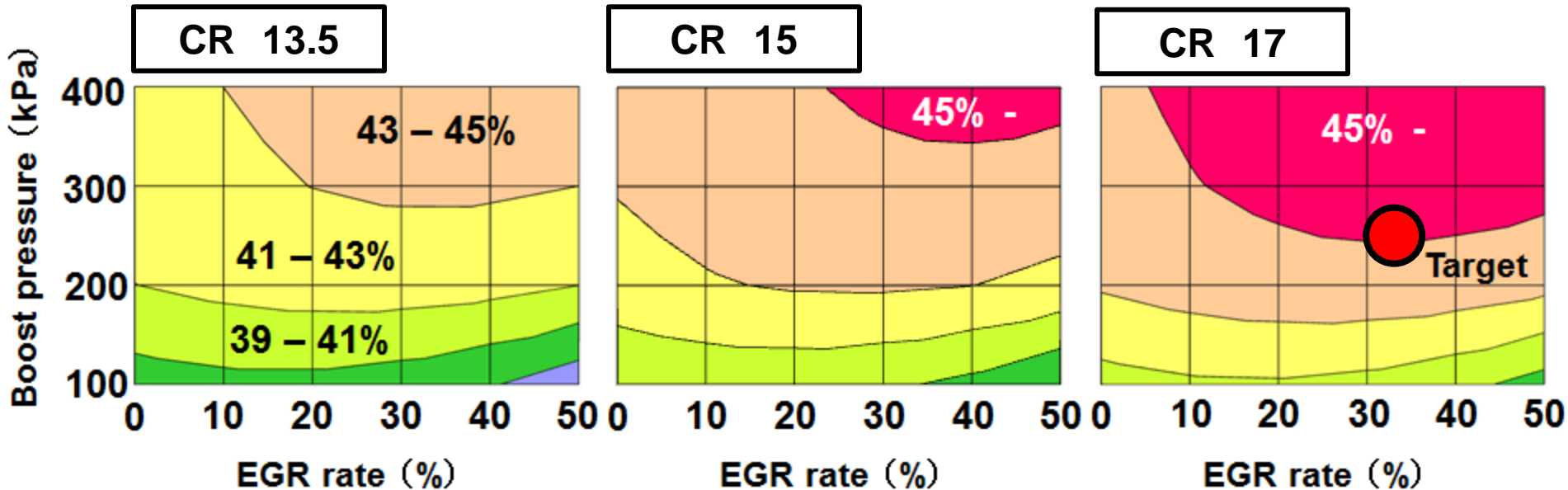
Intended Direction of This Research



How to Achieve Target Thermal Efficiency

Estimated Efficiency by Past Test Result and 1D Simulation

L4 2000cc
Ne=2000rpm



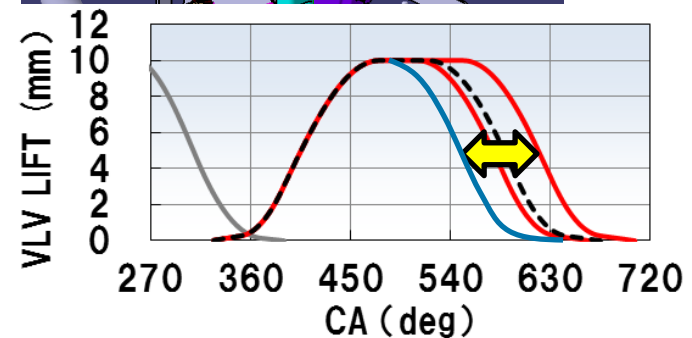
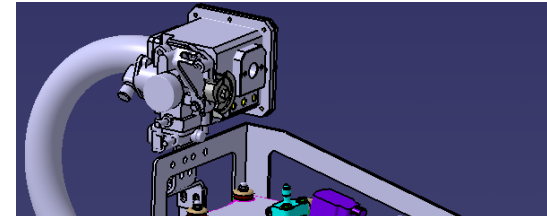
- Compression ratio (CR) : 17 or over
- Ignition timing : MBT
- EGR rate : 30% or more
- Boost pressure : 200 kPa or more

*FMEP: Mass-production L4 engine
*Ignition timing: MBT

Test System : Single-cylinder Engine

Engine specifications

Engine type	DOHC 4-valve Single-cylinder
Compression Ratio (CR)	13.5 -- 20.0
Inlet Valve Close @1mm	40,54,64,74,84° ABDC
Bore, Stroke (mm)	Φ81 , 96.6 -- 121.5 -- 162
S/B	1.2 -- 1.5 -- 2.0
Displacement Volume (cm ³)	499 -- 626 -- 835
Intake Port	Tumble Port
Air Supply	Super-charger
EGR Supply	LPL - EGR
Fuel Supply	PI / DI

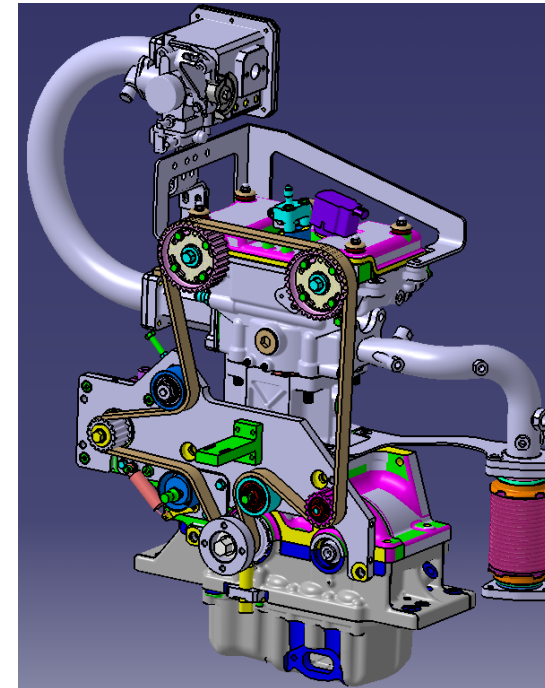


**Inlet Valve Open @1mm
-10deg ATDC (Fixed)**

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EGR Supply	LPL - EGR
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Stroke was changed by

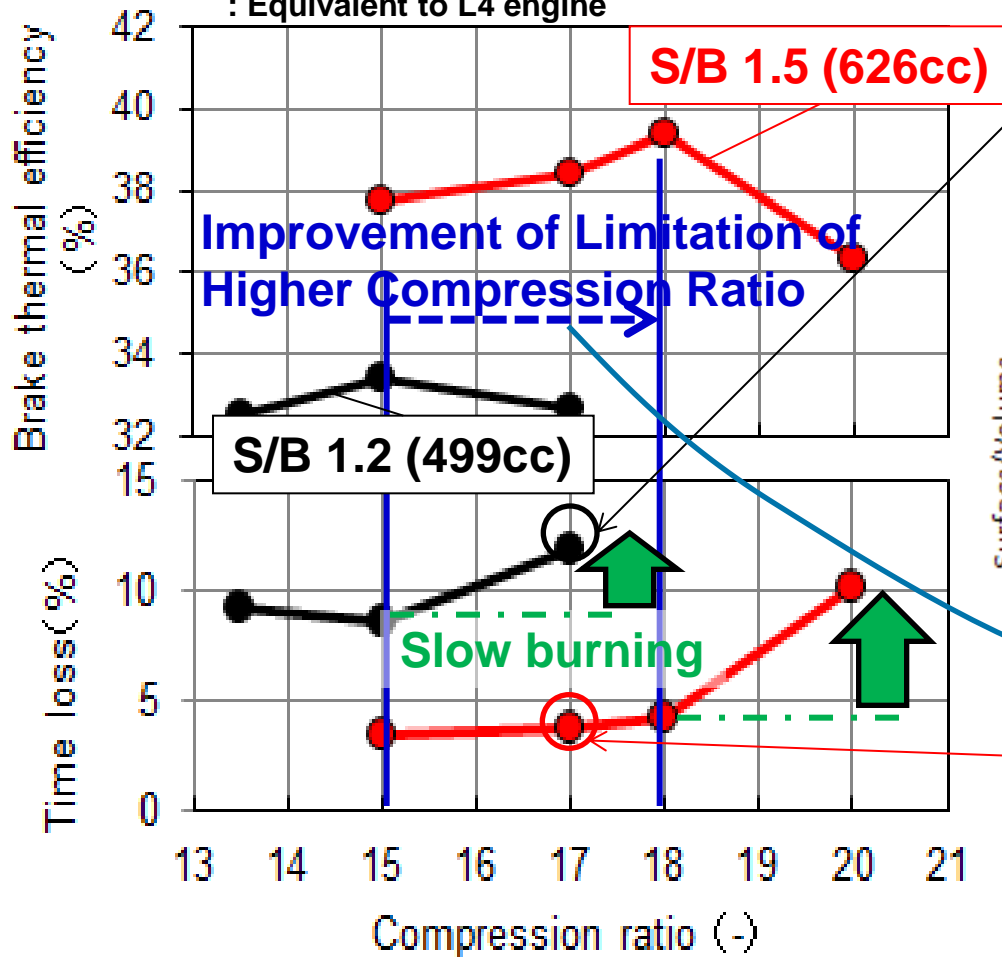
- **Crankshaft**
- **Connecting Rod**
- **Cylinder Sleeve**

Countermeasure of High Compression Ratio

1 Stroke-Bore (S/B) ratio

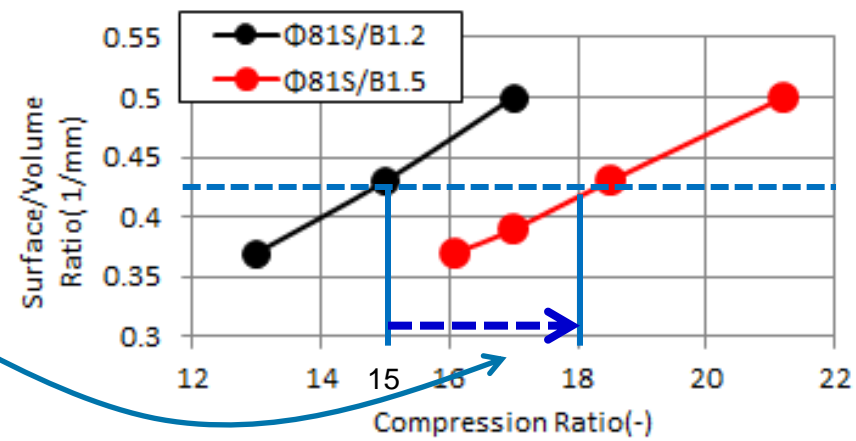
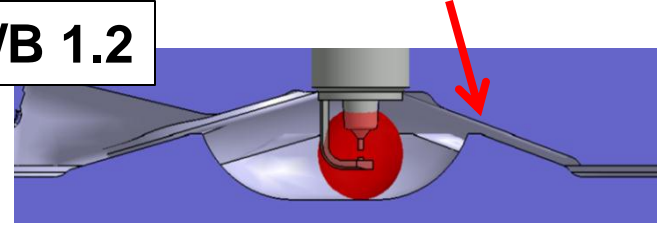
2000 rpm, IMEP 520 kPa, MBT, Port injection

*Thermal efficiency calculation FMEP, PMEP
: Equivalent to L4 engine

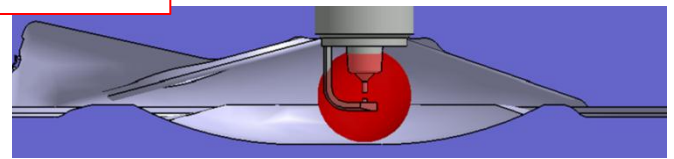


Slow burning occurred by narrow area of combustion chamber

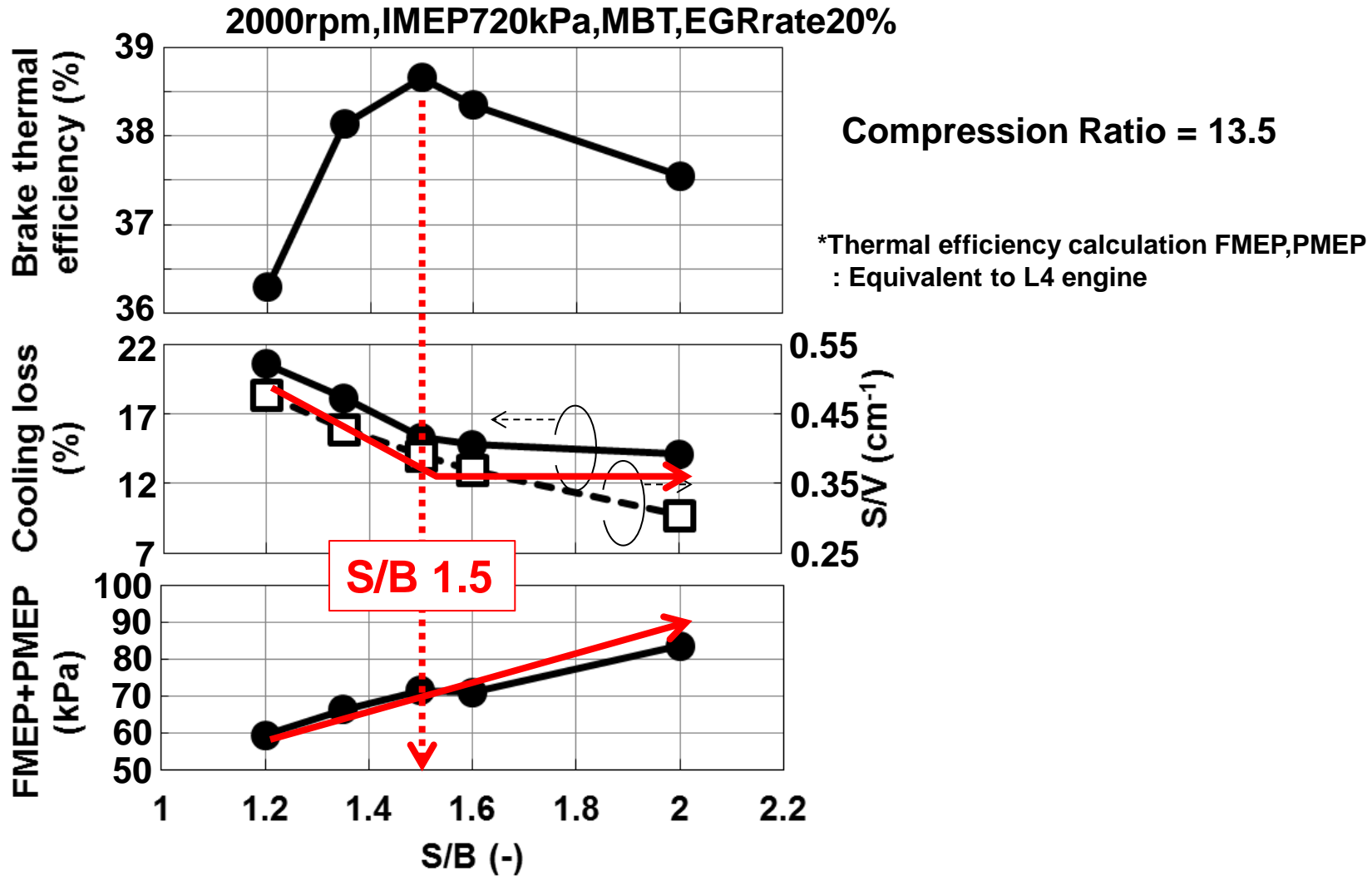
S/B 1.2



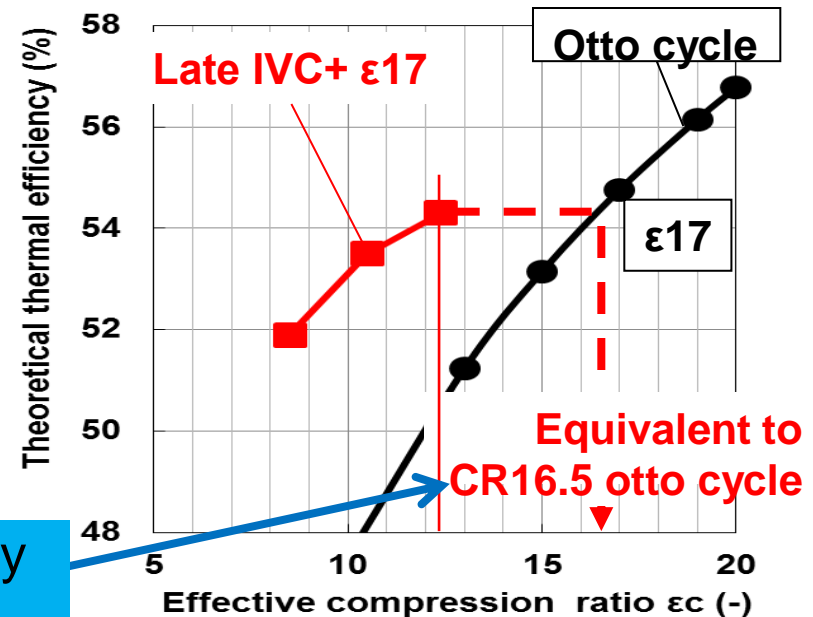
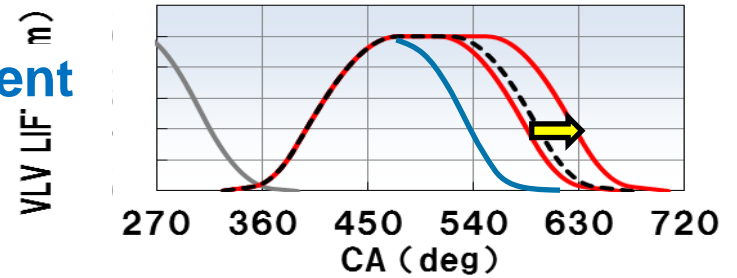
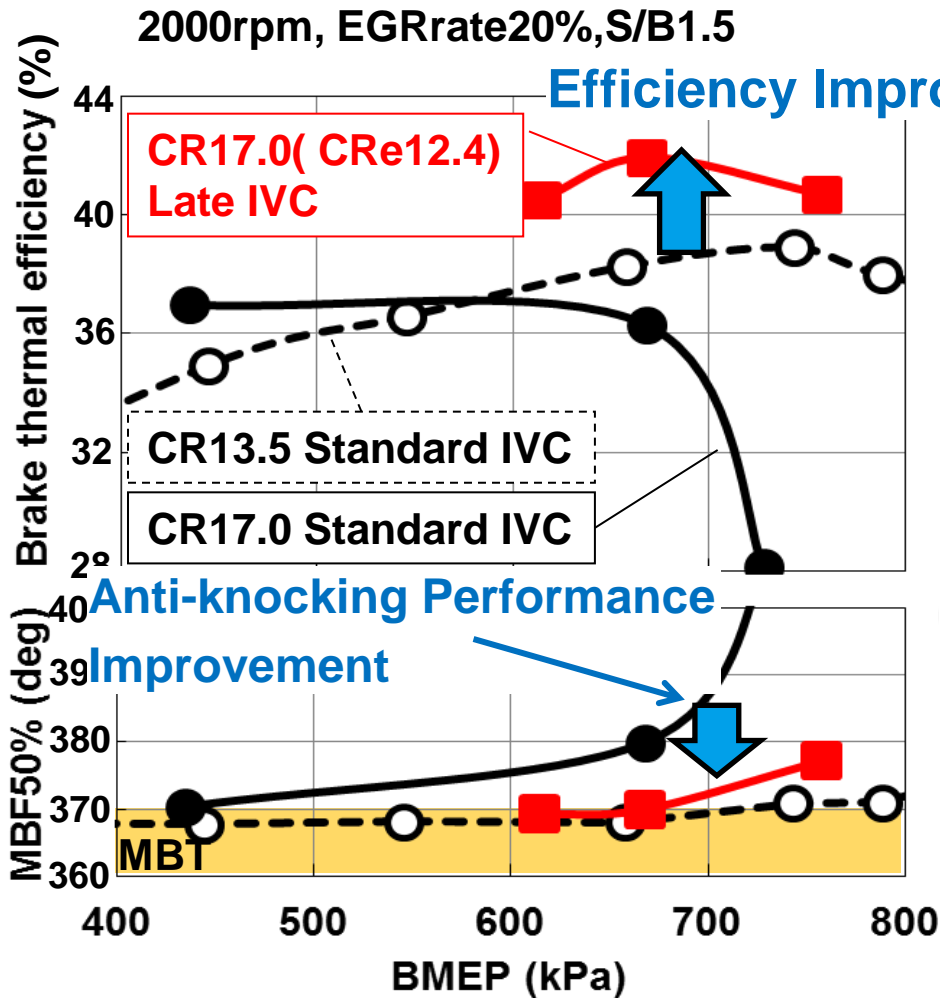
S/B 1.5



Influence of S/B to thermal efficiency



Countermeasure of High Compression Ratio 2 Effective Compression Ratio (Late Intake Valve Close)



Theoretical Thermal Efficiency
Equivalent to CR16.5

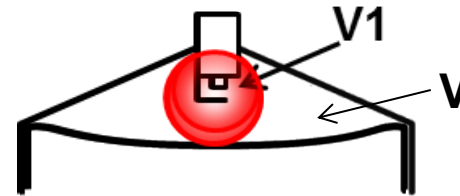
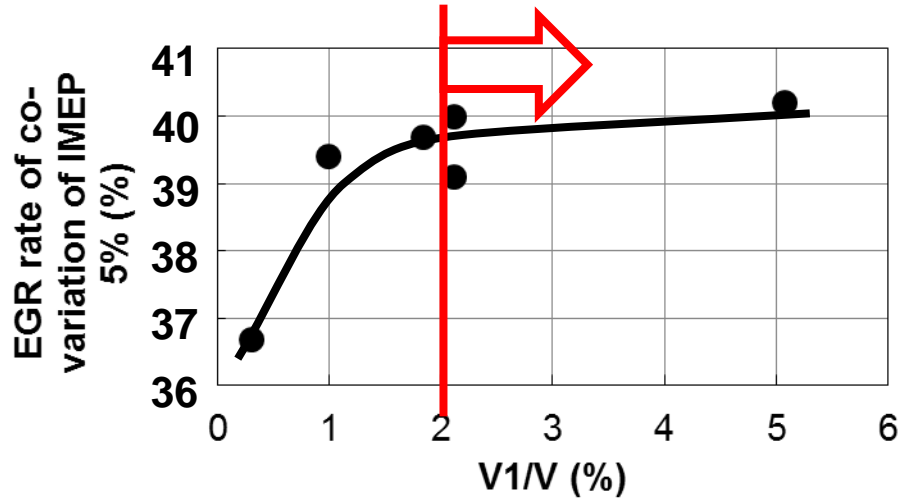
Countermeasure for High EGR Ratio

1 Flame Kernel Formation

Space Near Spark Plug Gap

- $V1 > 2\%$ of Combustion Chamber Volume at TDC

2000 rpm IMEP 810 kPa



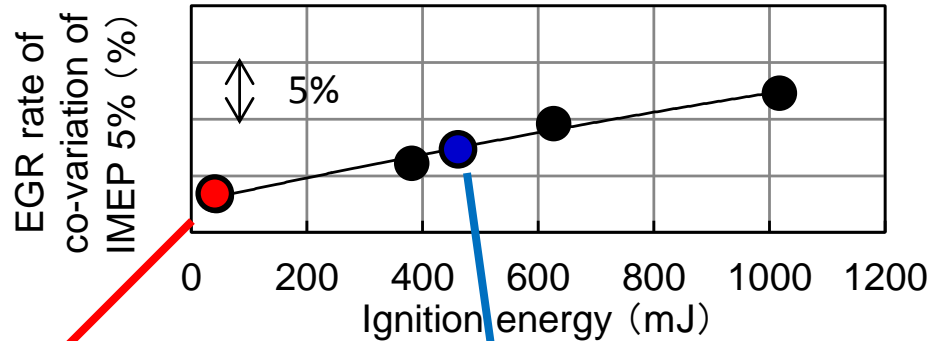
V : Combustion chamber volume at TDC
 $V1$: Volume of virtual sphere centering on Ignition-plug electrode with inflating to touch surface of piston or cylinder head

Countermeasure for High EGR Ratio

1 Flame Kernel Formation

High Energy Ignition

- Ignition Energy Extends EGR Limit
- Ignition Energy Set to 450mJ
 - Wear of Spark Plug
 - Power consumption

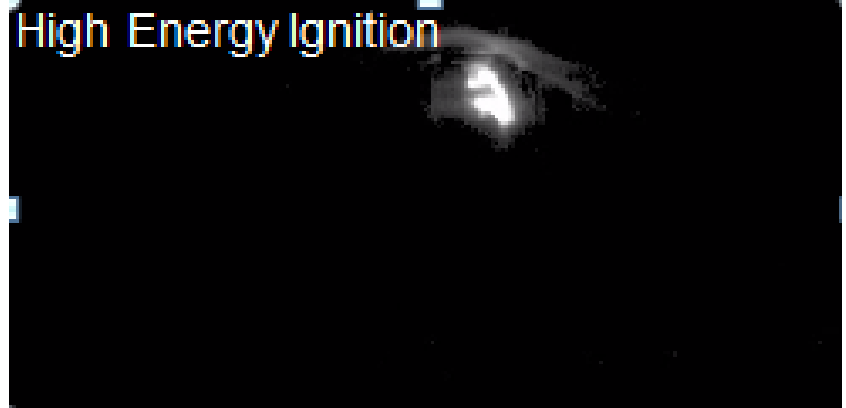


2000 rpm, IMEP 520 kPa, EGR Rate=20%, $\epsilon = 9.5$

Standard Ignition

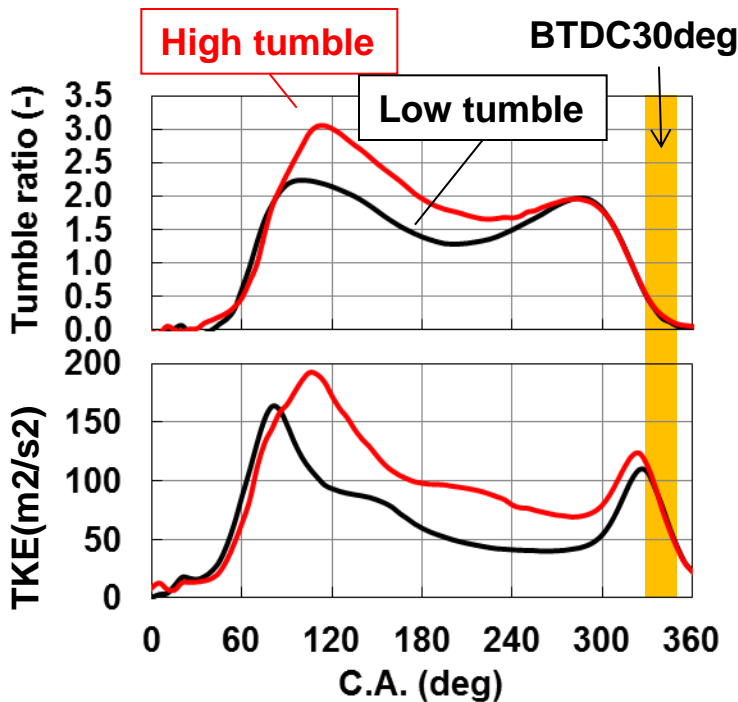


High Energy Ignition



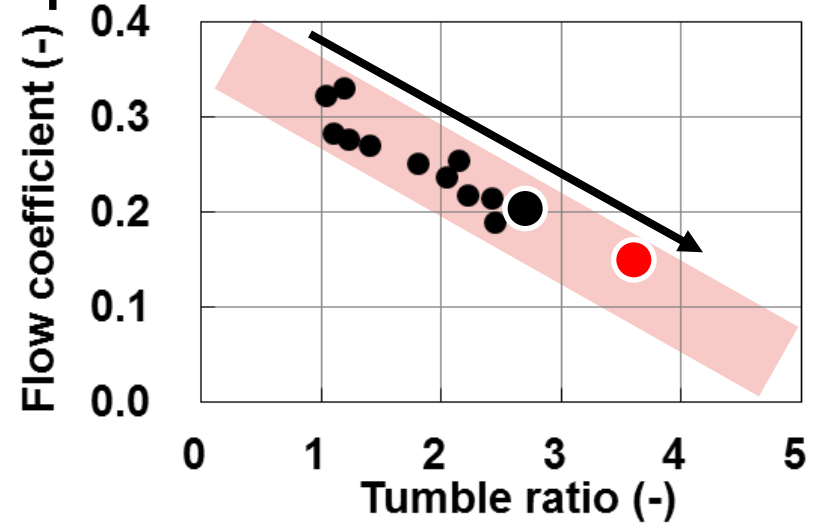
Countermeasure for High EGR Rate

2 High Turbulent Intensity - 3D Simulation Result

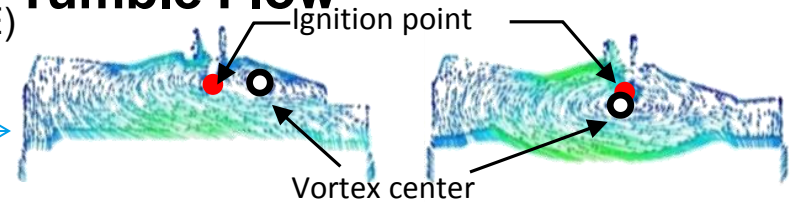


Higher Tumble Ratio Worsens Flow Coefficient

>> Higher Boosting Efficiency Requirement

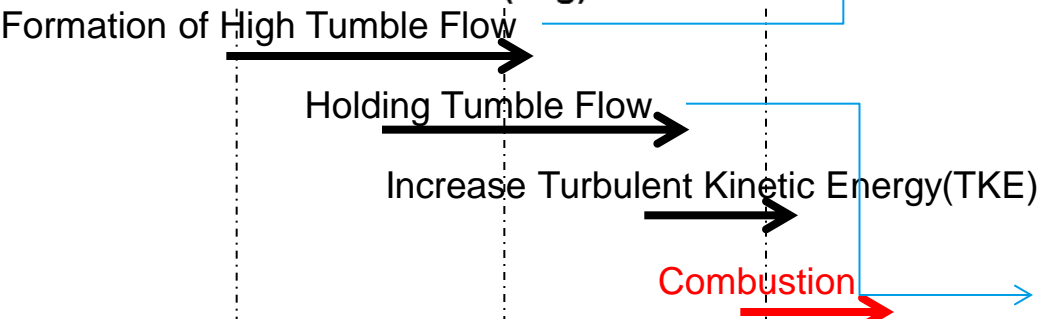


Piston Shape for Keep Tumble Flow



(a) Flat piston

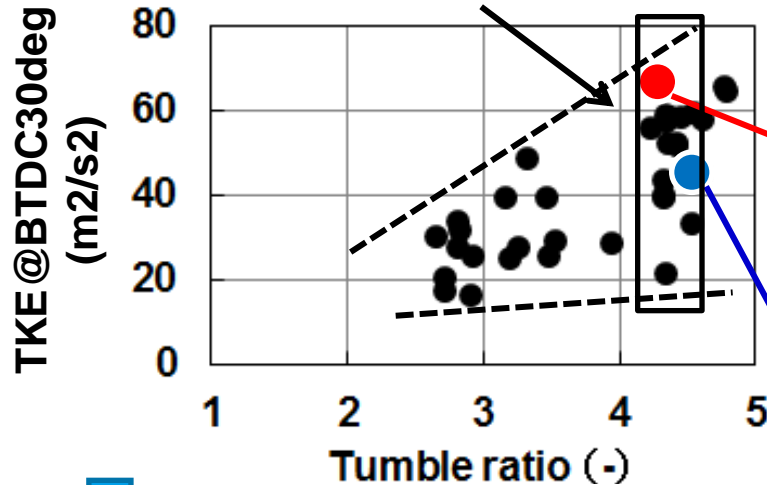
(b) Bowl-shaped piston



Countermeasure for High EGR Rate

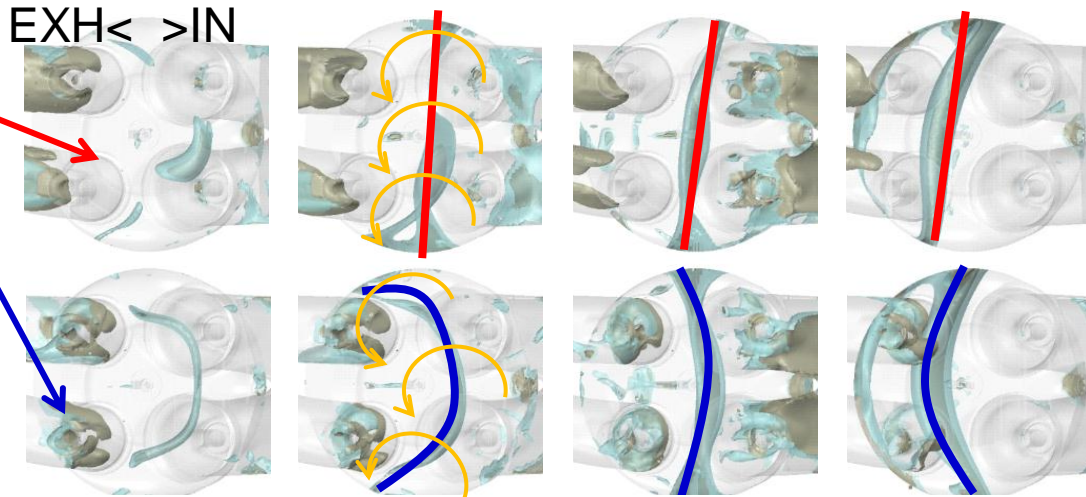
2 High Turbulent Intensity - 3D Simulation Result

Same Tumble Ratio,
TKE Varied



High TKE:<Stable>

Small Change In Center Axis of Tumble Flow



BTDC
240deg

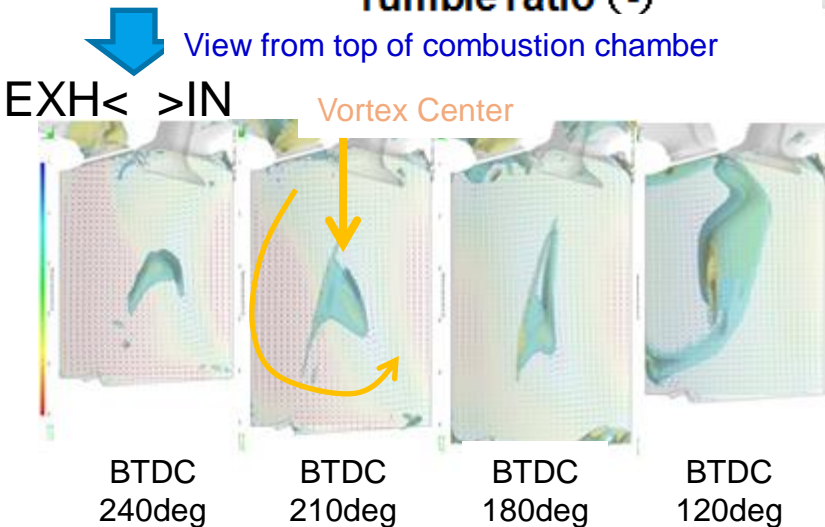
BTDC
210deg

BTDC
180deg

BTDC
120deg

Low TKE:<Unstable>

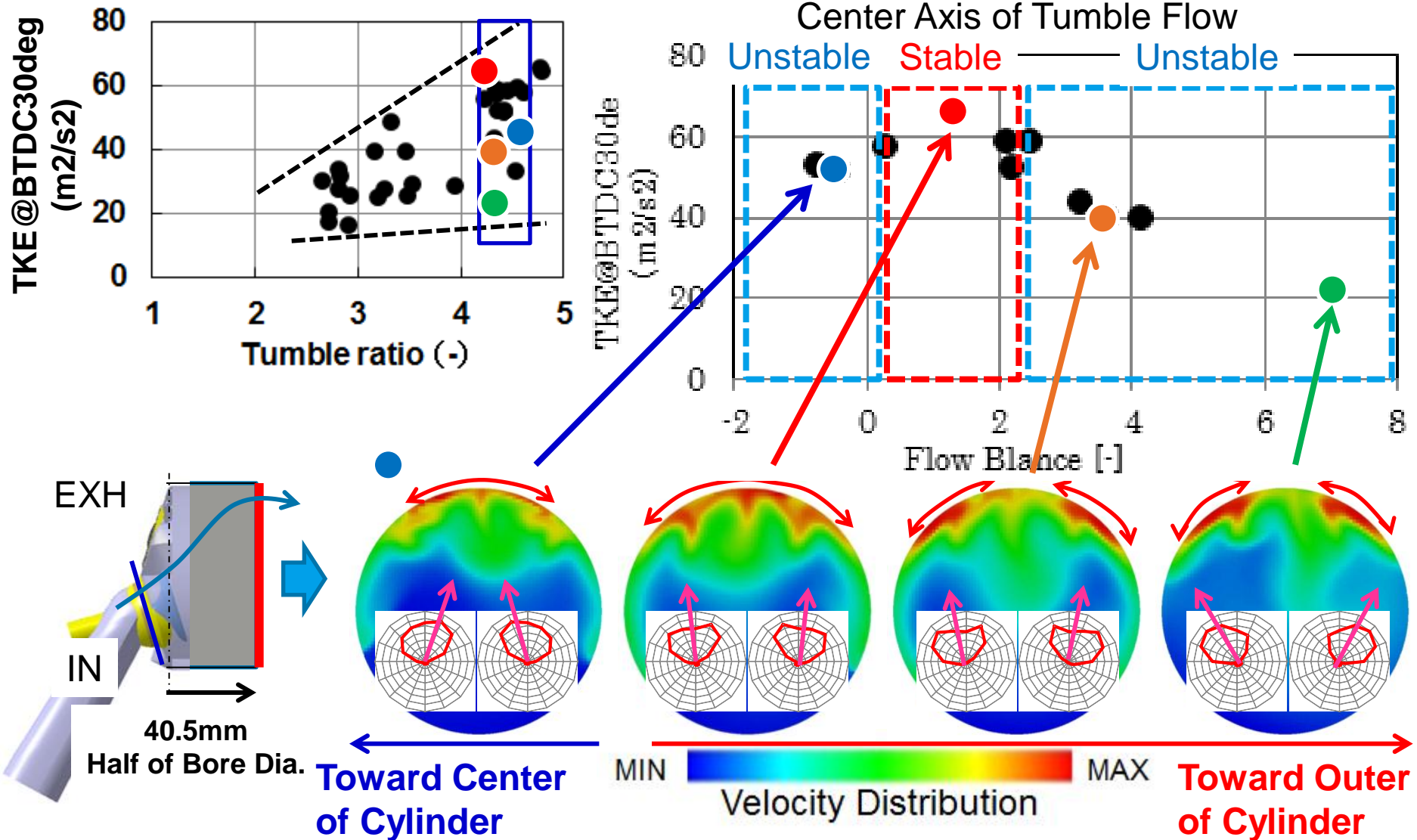
Large Change In Center Axis of Tumble Flow



Stable Center Axis of Tumble Flow Make
Higher TKE

Countermeasure for High EGR Rate

2 High Turbulent Intensity - 3D Simulation Result

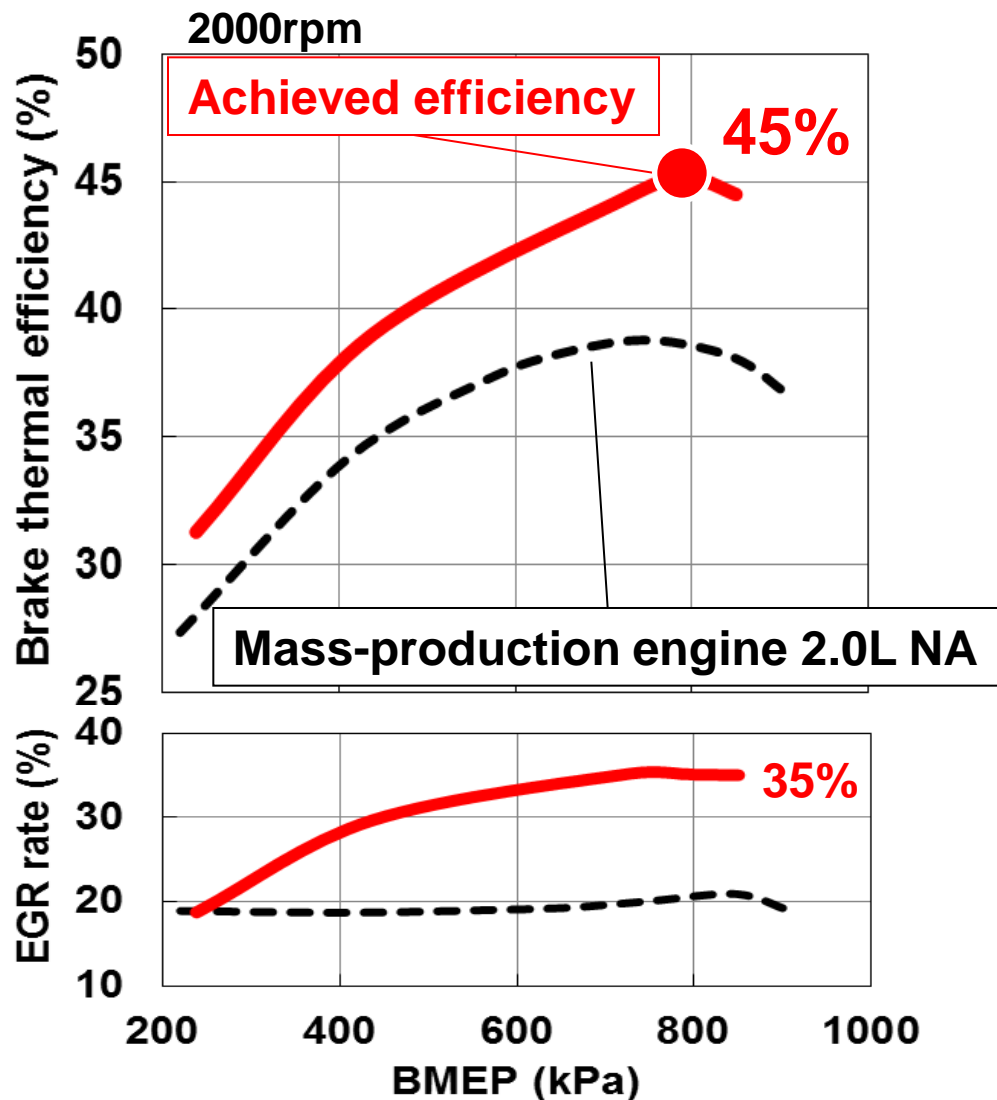


Brake Thermal Efficiency Achieved : Single Cylinder Engine

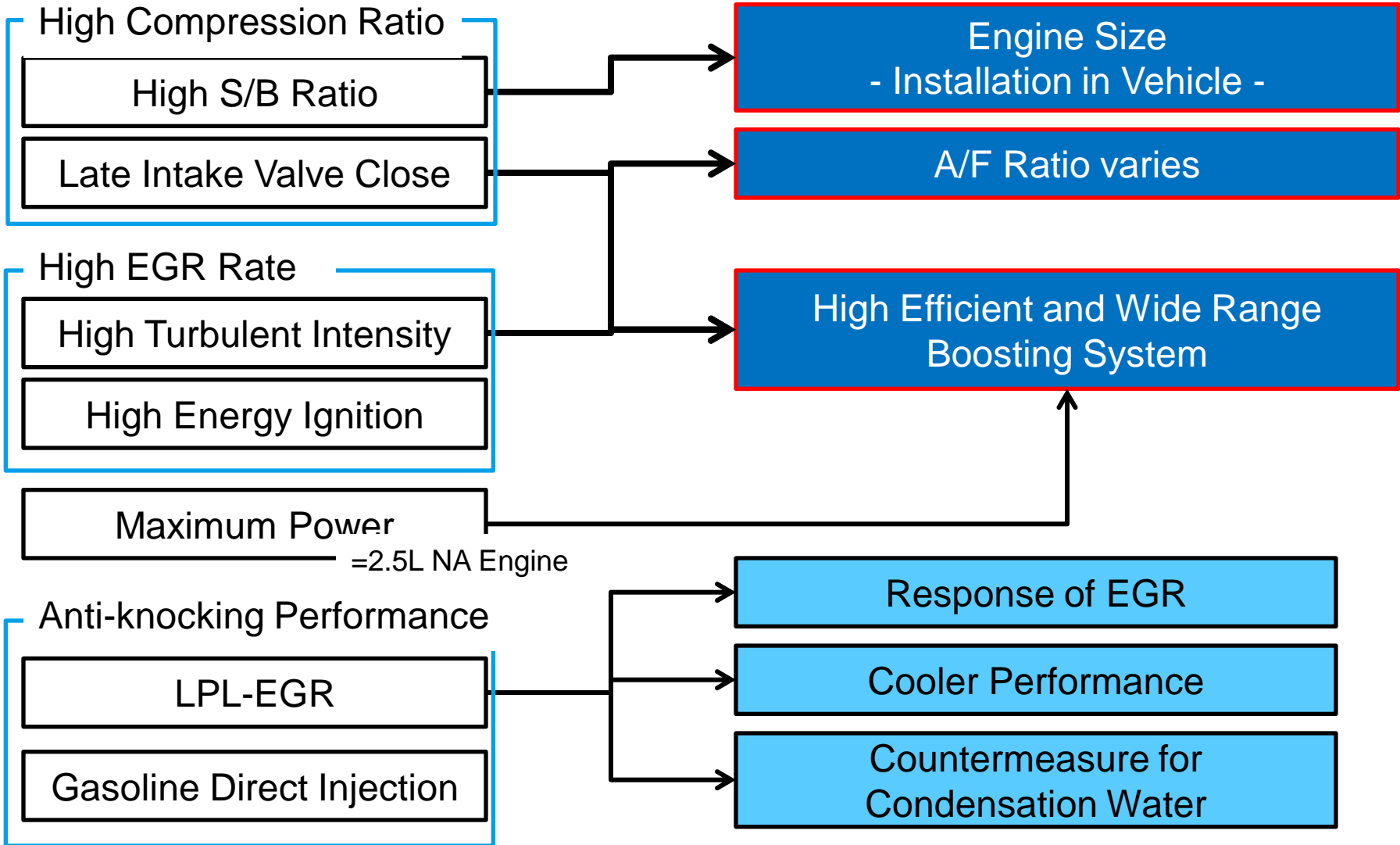
Engine specifications

Engine type	DOHC 4-valve
Bore, Stroke (mm)	Φ81 , 162
S/B	1.5
Displacement volume (cm ³)	626
Compression ratio	17.0
Effective compression ratio	12.4
Intake port	Tumble port
Piston shape	Bowl shape
Ignition energy	450 mJ
Air supply	Super-charger
Fuel supply	DI

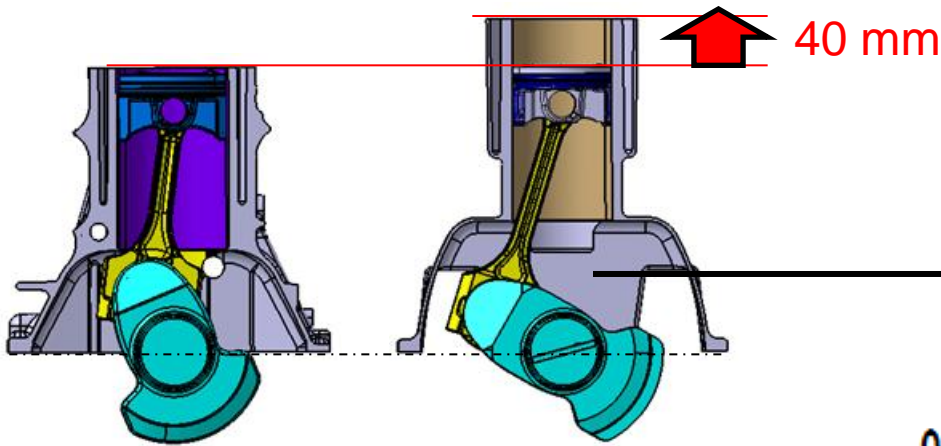
*Thermal efficiency calculation FMEP,PMEP
: Equivalent to L4 engine



Engine System Design



Engine Height Setting



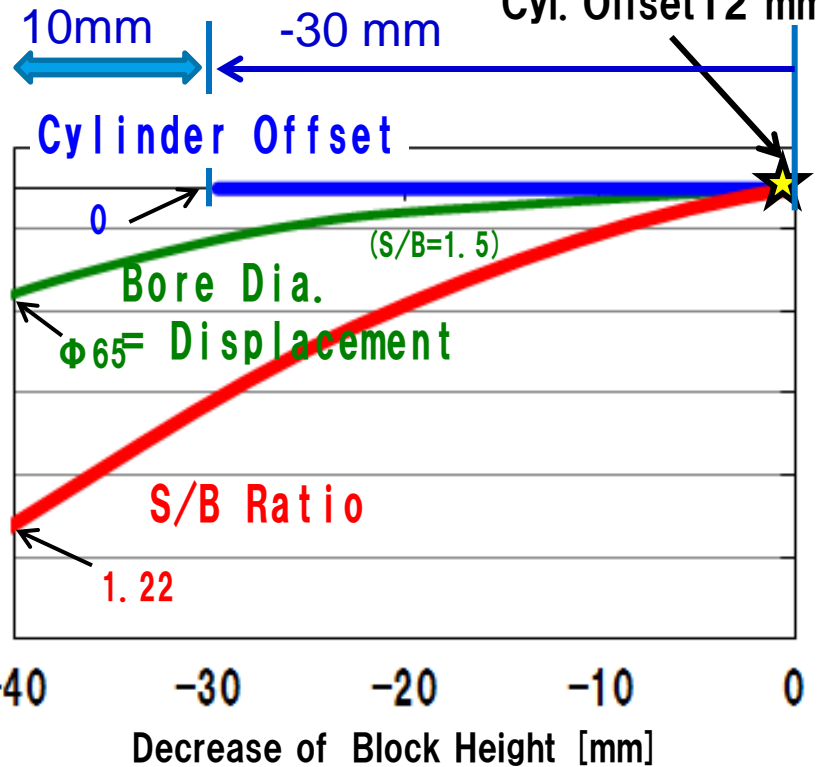
Conventional
S/B Ratio 1.2

$\eta_e 45\%$
S/B Ratio 1.5

S/B Ratio Changes from 1.2 to 1.5

- Block Height Increase 40 mm

<Base>
S/B Ratio 1.5
Bore Dia. $\Phi 81$ mm
Cyl. Offset 12 mm



Factors Affecting Block Height

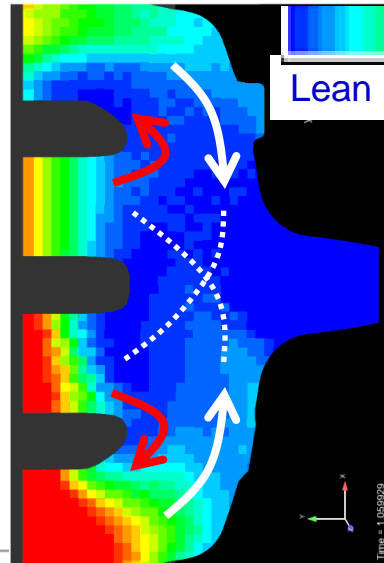
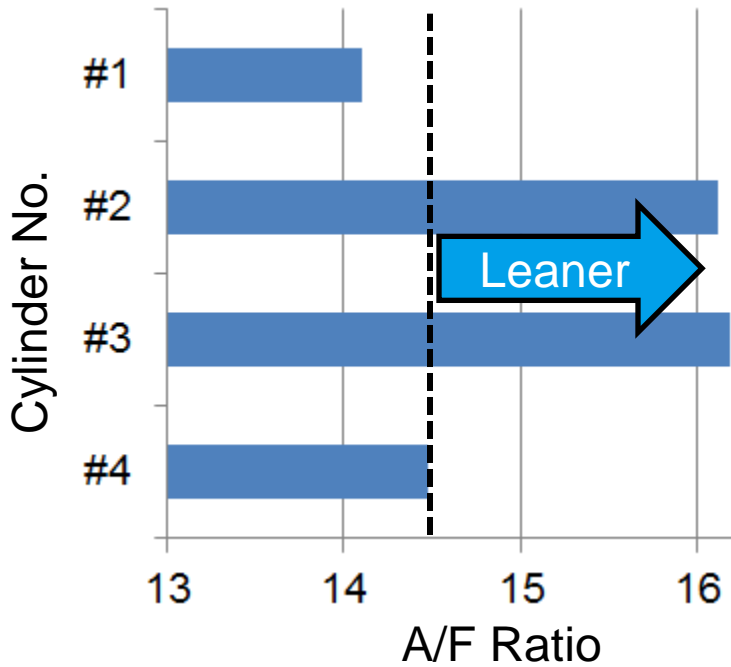
- S/B Ratio
- Cylinder Offset
- Bore Diameter



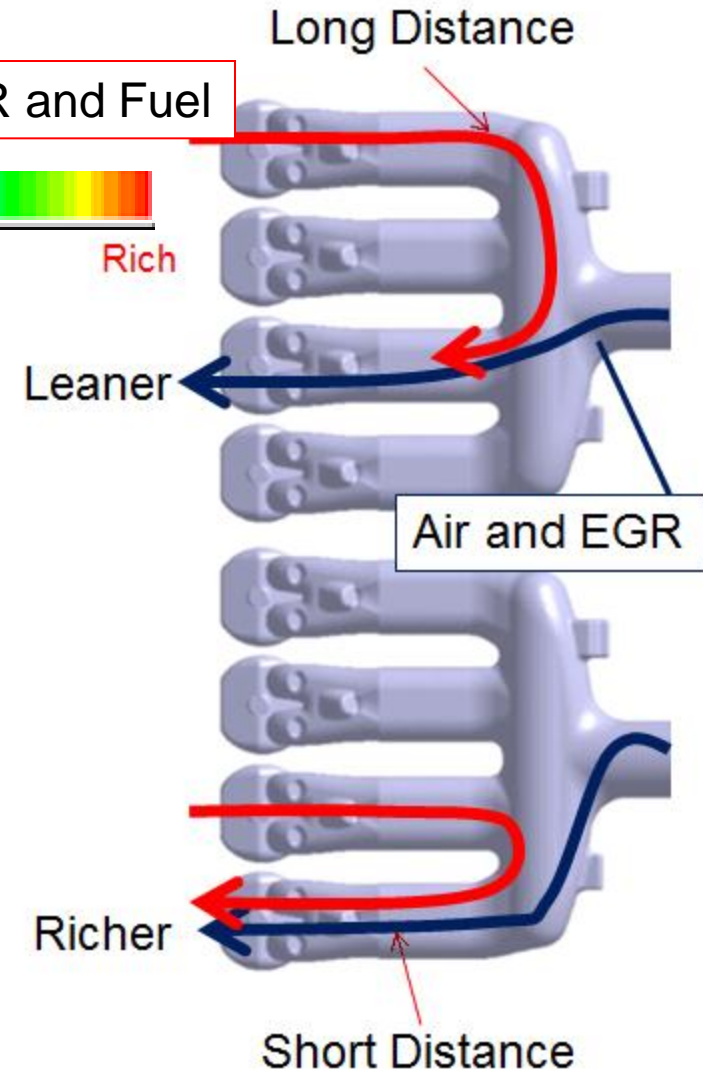
Eliminate Cylinder Offset to Give Priority to Efficiency-improving Benefit of S/B Ratio

A/F Ratio Varies

2000 rpm, IMEP 520 kPa, EGR 0%

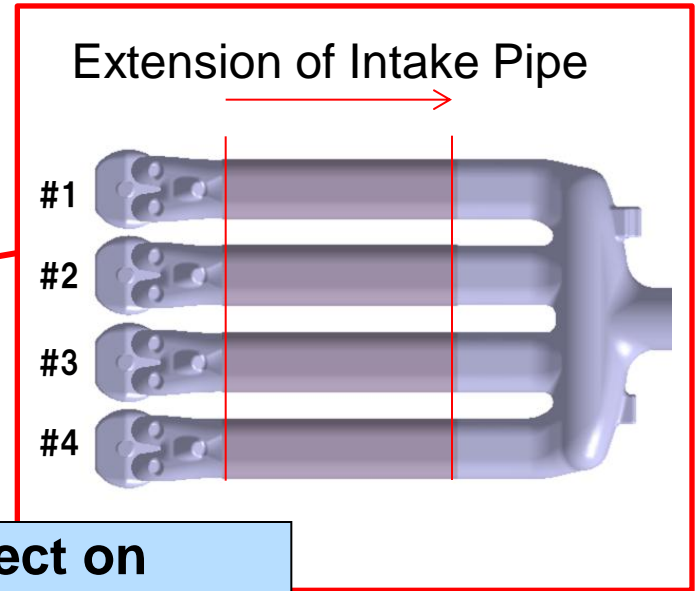
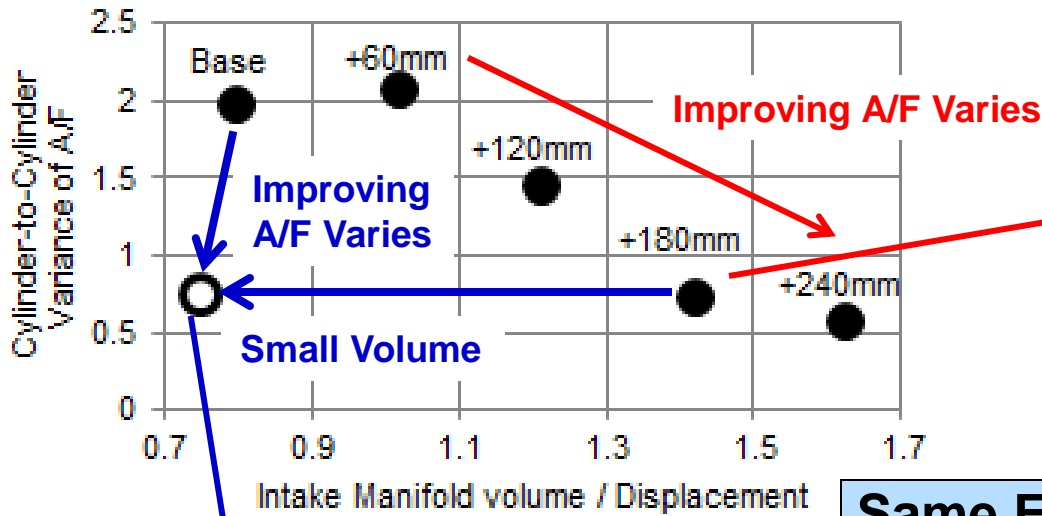


Air, EGR and Fuel



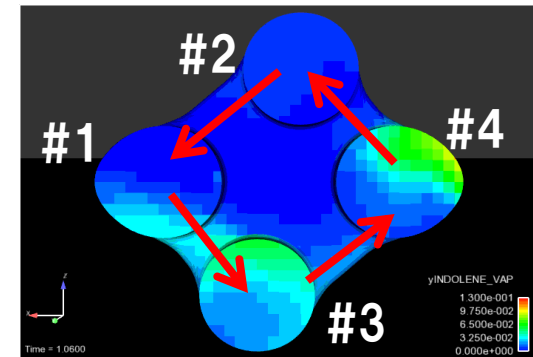
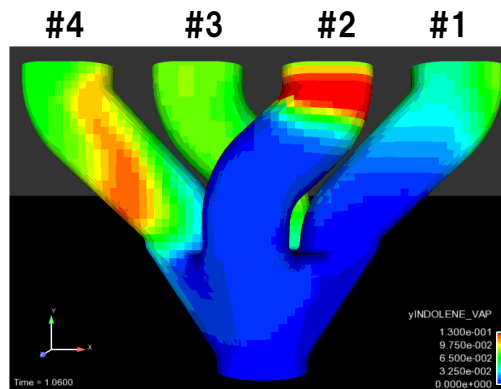
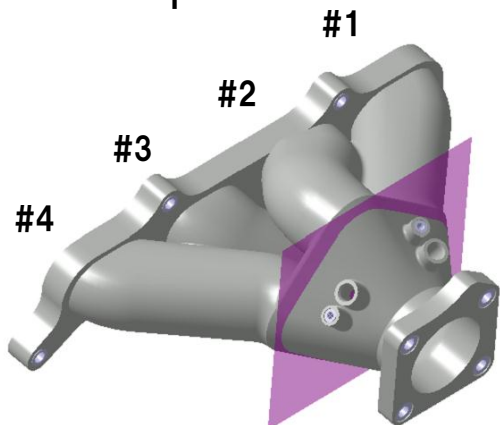
Miller Cycle Cause A/F Varies

A/F Ratio Varies / Countermeasure

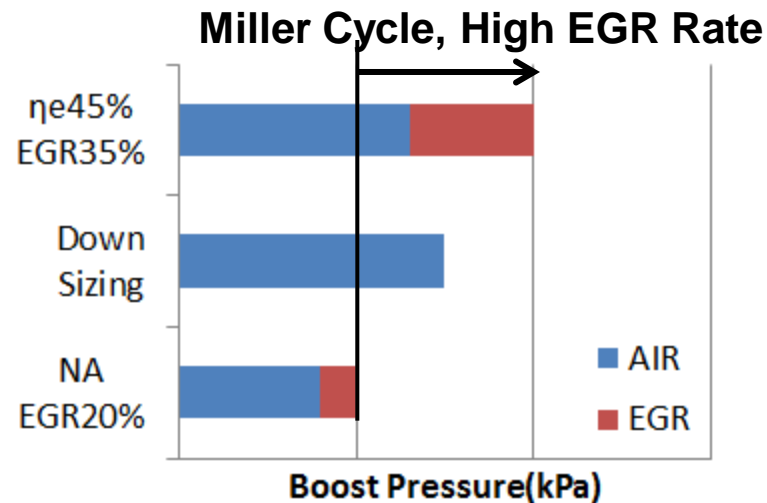
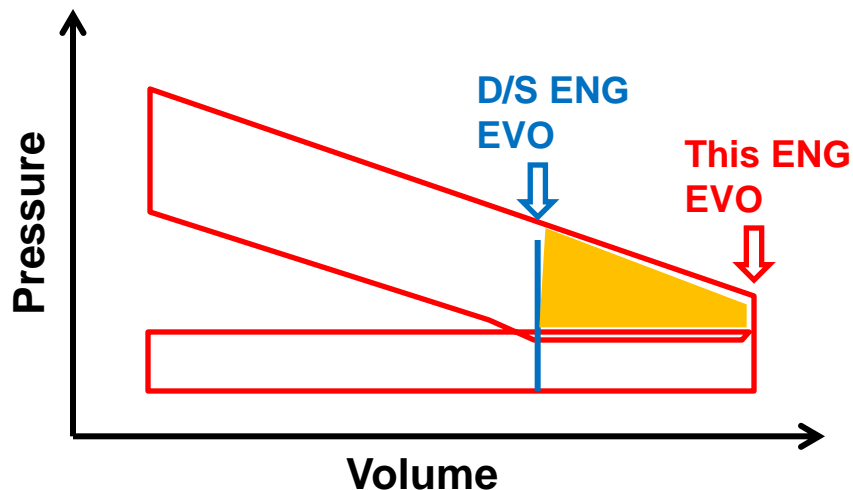


Same Effect on Less Intake Volume

Intake Pipes Assembled in Firing Order

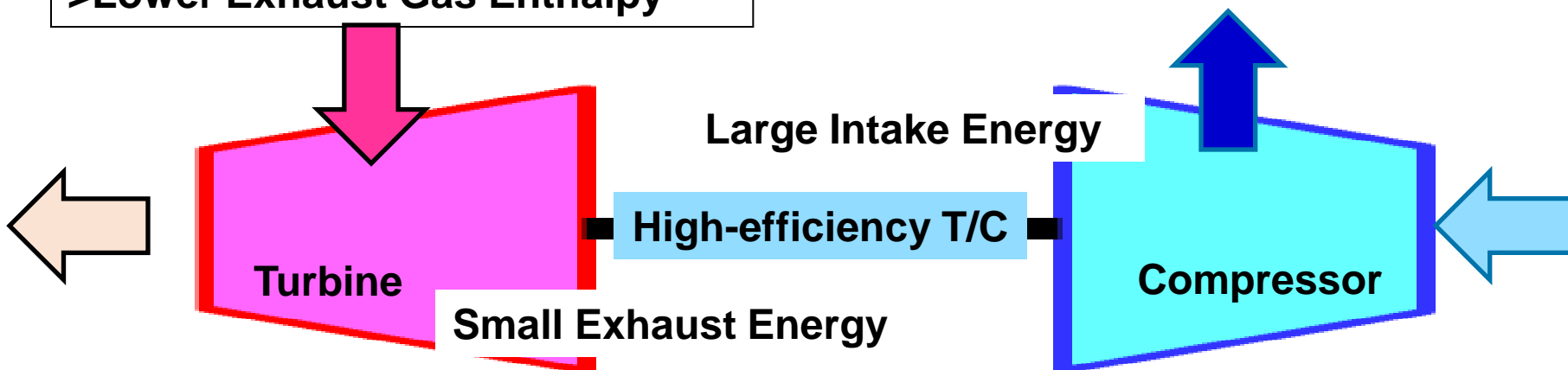


Examination of Boosting System Specifications

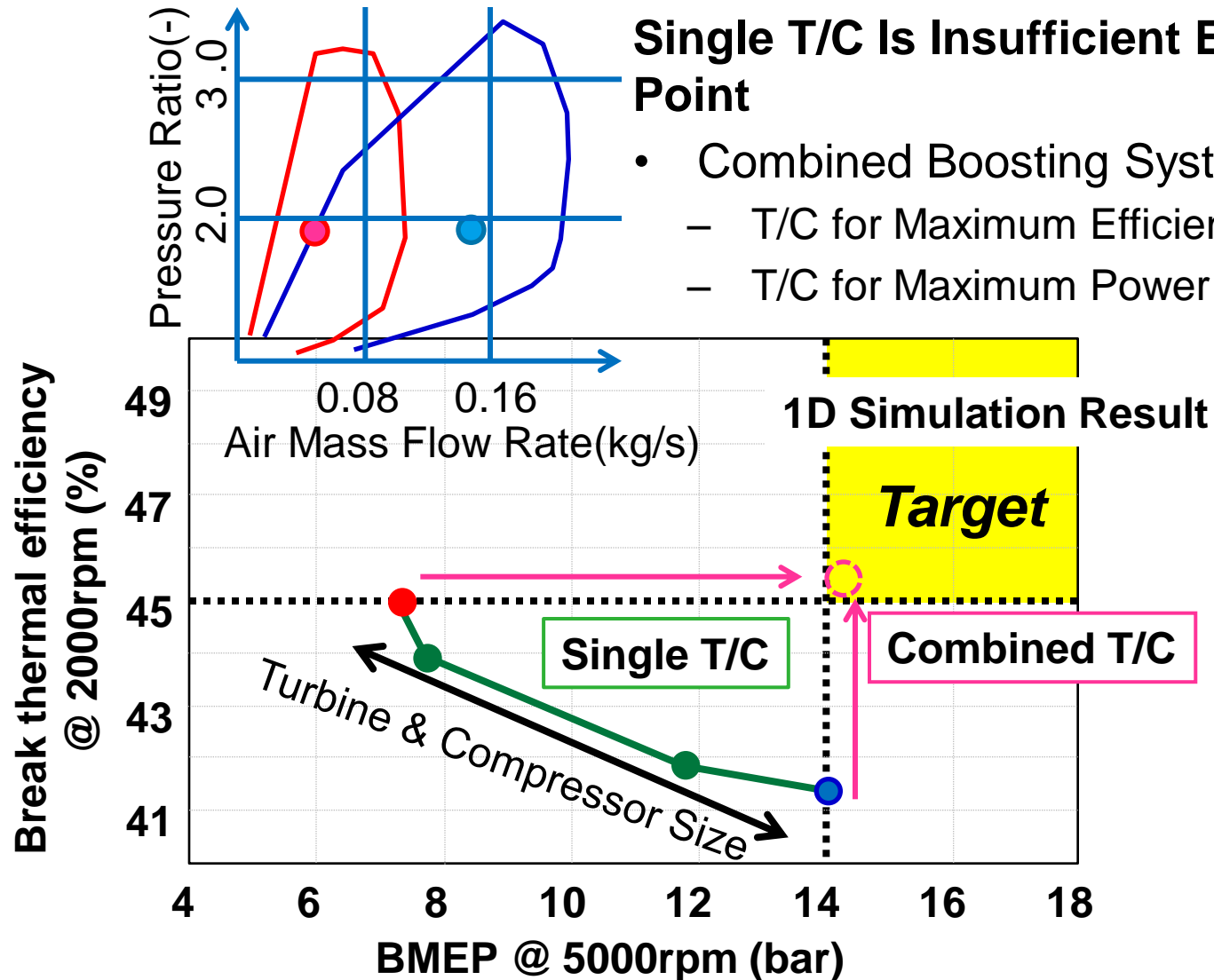


High EGR Rate and High Expansion Ratio
 >Lower Exhaust Gas Enthalpy

Miller Cycle and High EGR Rate
 >High Boost Pressure Is Required



Examination of Boosting System Specifications



3. How to Achieve Brake Thermal Efficiency 45%

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4. Conclusion

Specifications of 45% Brake Thermal Efficiency on Single Cylinder Engine

Higher Compression Ratio : Compression Ratio 17

- Late Intake Valve Close--- Effective Compression Ratio 12.4
- Long Stroke --- Stroke-Bore Ratio 1.5

Higher EGR Rate : EGR Rate 35%

- Ensuring Space around Ignition Point --- 2% Volume of TDC's Combustion Chamber Volume
- High Energy Ignition --- 450mJ
- High Turbulent Kinetic Energy --- High Tumble Ratio Port, Keeping Tumble Flow Shape of Combustion Chamber

Multi Engine Application

Increased Engine Height Due to High Stroke-Bore Ratio

- 0 Cylinder Offset to Restrict Engine Height Increase to 10mm

Countermeasure for A/F varies caused by Late Intake Valve Close

- Firing Order Arranged Intake Manifold

High Efficiency and Wide range Boosting System is Needed

- Combined T/C

Conclusion

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Thank you for your kind attention.

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